



Non-perturbative collective inertias for fission: A comparative study

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ABSTRACT

The non-perturbative method to compute Adiabatic Time Dependent Hartree Fock Bogoliubov (ATDHFB) collective inertias is extended to the Generator Coordinate Method (GCM) in the Gaussian overlap approximation (GOA) including the case of density dependent forces. The two inertias schemes are computed along the fission path of the ^{234}U and compared with the perturbative results. We find that the non-perturbative schemes predict very similar collective inertias with a much richer structure than the one predicted by perturbative calculations. Moreover, the non-perturbative inertias show an extraordinary similitude with the exact GCM inertias computed numerically from the energy overlap. These results indicate that the non-perturbative inertias provide the right structure as a function of the collective variable and only a phenomenological factor is required to mock up the exact GCM inertia, bringing new soundness to the microscopic description of fission.

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1. Introduction

Despite its discovery dates back almost 80 years, fission still remains a major challenge for nuclear theory [1]. The lack of a feasible full quantum formalism describing the evolution of the nucleus from the ground state to scission enforces the adoption of different approximations, which in turn provide a theoretical framework for the estimation of fission properties in nuclei. For instance, the starting point in any traditional energy density functional calculation is the original assumption that fission can be described using a reduced set of collective variables [2,3]. Within this approximation the fission probability is obtained as the probability of the nucleus to tunnel under the fission barrier, which is driven by the potential energy surface (PES) and the collective inertias felt by the nucleus in its way to scission [4,5]. Both quantities, together with the collective ground-state energy, enter in the collective action integral allowing for the calculation of the spontaneous fission lifetime by means of the semiclassical Wentzel–Kramers–Brillouin (WKB) approach.

A sound calculation of the PES, collective ground-state energy and collective inertias is thus essential for a proper estimation

of fission lifetimes [1,6]. If the formalism that shall be used in the calculation of the first two quantities is well established, the same cannot be claimed for the collective inertias. Nowadays two theoretical frameworks allow for a derivation of a collective Schrödinger equation and its associated inertia: the Adiabatic Time Dependent Hartree Fock Bogoliubov (ATDHFB) formalism and the Generator Coordinate Method (GCM) with the Gaussian overlap approximation (GOA) [1]. In both approaches the collective inertias can be written in terms of the collective momentum operators, which in turn can be related to the linear response matrix (LRM) and its inverse when acting on Hartree Fock Bogoliubov (HFB) wave functions. Given the whopping number of two-quasiparticle elementary excitations in realistic applications to fission, the dimensionality of the LRM is very high and therefore its inverse is difficult to evaluate. To avoid this bottleneck the assumption of diagonal dominance of the LRM is often used, leading to the traditional perturbative cranking formulas for the collective inertias involving denominators composed of two quasiparticle energies. A better approximation to the exact expression of the collective inertias was introduced in [7] (see also [8]), where the collective momentum operator is computed in terms of the derivatives of the density and pairing tensor with respect of the collective variables. This non-perturbative cranking calculation of the collective inertias, implemented in the ATDHFB approach, showed that the numerical treatment of the derivatives gives rise to a less adiabatic

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behavior of the collective inertias in comparison to the perturbative calculation.

It follows then that there are two different sources of uncertainty in the calculation of the collective inertias: one related to the choice of the theoretical framework (ATDHFB vs GCM-GOA) and the other related to the approximations involved in the numerical evaluation of the inertias (exact vs non-perturbative vs perturbative). The purpose of this paper is then twofold: (i) to introduce for the first time the non-perturbative scheme in the GCM-GOA framework and (ii) compute the exact GCM-GOA collective inertias and use this result to study the suitability of both the ATDHFB and the GCM-GOA non-perturbative schemes. Using the actinide ^{234}U as a test case, we will show that, as the level of approximation improves, the results obtained in the ATDHFB and the GCM schemes naturally converge towards the same solution of the collective inertias, bringing new solidity to the theoretical description of fission. The present results represent a step forward in the microscopic description of fission providing the method with the credibility required to answer questions like the very existence of nuclei beyond oganesson [9].

2. Methodology

This section is devoted to the derivation of the different expressions used for the calculation of the collective inertias. The key element is the momentum operator \hat{P}_q associated to the collective variable q which is derived in the quasiparticle representation in section 2.1. This quantity is then used to obtain the non-perturbative expression of the GCM-GOA mass in section 2.2 while the extension to density dependent forces is presented in section 2.3. In section 2.4 we discuss how to compute the exact GCM-GOA mass using the numerical derivatives of the exact Hamiltonian and norm kernels. In section 2.5 we will briefly review the derivation of the ATDHFB non-perturbative formula. Section 2.6 is devoted to obtaining the explicit expression of the perturbative masses, both in the GCM-GOA and ATDHFB framework. Finally, the connection between collective inertias and moments of inertia is presented in section 2.7.

2.1. Momentum operator

Given a collective variable q like, for instance, the quadrupole moment, its associated collective moment \hat{P}_q can be defined through the relation (we use $\hbar = 1$ in the following)

$$i\hat{P}_q|\Phi(q)\rangle = \frac{\partial}{\partial q}|\Phi(q)\rangle = \lim_{\delta q \rightarrow 0} \frac{|\Phi(q + \delta q)\rangle - |\Phi(q)\rangle}{\delta q}. \quad (1)$$

Both $|\Phi(q + \delta q)\rangle$ and $|\Phi(q)\rangle$ are HFB wave functions satisfying the HFB equation with the corresponding constraints $\langle\Phi(q + \delta q)|\hat{Q}_{20}|\Phi(q + \delta q)\rangle = q + \delta q$ and $\langle\Phi(q)|\hat{Q}_{20}|\Phi(q)\rangle = q$, respectively. To evaluate $|\Phi(q + \delta q)\rangle$ in terms of $|\Phi(q)\rangle$ we use linear response theory in the quasiparticle representation. We notice that $|\Phi(q + \delta q)\rangle$ and $|\Phi(q)\rangle$ are related by a Thouless transformation that, for infinitesimal δq , can be written as

$$|\Phi(q + \delta q)\rangle = |\Phi(q)\rangle + \delta q \hat{Z}(q)|\Phi(q)\rangle + O(\delta q^2), \quad (2)$$

with

$$\hat{Z}(q) = \frac{1}{2} \sum_{\mu\nu} Z_{\mu\nu}(q) \beta_{\mu}^{\dagger}(q) \beta_{\nu}^{\dagger}(q). \quad (3)$$

On the other hand, $|\Phi(q + \delta q)\rangle$ satisfies the HFB equation with constraints

$$\langle\Phi(q + \delta q)| \left[\hat{H} - \sum_j \lambda_j(q + \delta q) \hat{Q}_j \right] \beta_{\mu}^{\dagger} \beta_{\nu}^{\dagger} |\Phi(q + \delta q)\rangle = 0, \quad (4)$$

where the quasiparticles creation operators above are defined at deformation $q + \delta q$

$$\beta_{\mu}^{\dagger}(q + \delta q) = \beta_{\mu}^{\dagger}(q) + \delta q \sum_{\mu'} Z_{\mu'\mu}^* \beta_{\mu'}^{\dagger}(q) + O(\delta q^2). \quad (5)$$

Expanding in powers of δq we obtain at zero order

$$\langle\Phi(q)| \left[\hat{H} - \sum_j \lambda_j(q) \hat{Q}_j \right] \beta_{\mu}^{\dagger}(q) \beta_{\nu}^{\dagger}(q) |\Phi(q)\rangle = 0, \quad (6)$$

which is an identity because $|\Phi(q)\rangle$ is the constrained HFB solution at deformation q . At first order in δq the following identity has to be satisfied

$$\frac{1}{2} \langle \hat{Z}^{\dagger} \Delta \hat{H}' \beta_{\mu}^{\dagger} \beta_{\nu}^{\dagger} \rangle + \frac{1}{2} \langle \Delta \hat{H}' \beta_{\mu}^{\dagger} \beta_{\nu}^{\dagger} \hat{Z} \rangle = \sum_j \frac{\partial \lambda_j}{\partial q} (Q_j)_{\mu\nu}^{20*}, \quad (7)$$

as well as its complex conjugated. In the above expression $\Delta \hat{O} = \hat{O} - \langle \hat{O} \rangle$, $(Q_j)_{\mu\nu}^{20*} = \langle \beta_{\nu} \beta_{\mu} \hat{Q}_j \rangle$ is the 20 part of the operator \hat{Q}_j , and $\hat{H}' = \hat{H} - \sum_j \lambda_j \hat{Q}_j$. Introducing the matrices

$$A_{\mu\nu\mu'\nu'} = \langle \beta_{\nu} \beta_{\mu} \Delta \hat{H}' \beta_{\mu'}^{\dagger} \beta_{\nu'}^{\dagger} \rangle, \quad (8a)$$

$$B_{\mu\nu\mu'\nu'} = \langle \beta_{\nu} \beta_{\mu} \beta_{\nu'} \beta_{\mu'} \Delta \hat{H}' \rangle, \quad (8b)$$

with the properties $A_{\mu'\nu'\mu\nu} = A_{\mu\nu\mu'\nu'}^*$ and $B_{\mu'\nu'\mu\nu} = B_{\mu\nu\mu'\nu'}$, Eq. (7) becomes

$$\sum_{\mu' < \nu'} Z_{\mu'\nu'}^* A_{\mu'\nu'\mu\nu} + Z_{\mu'\nu'} B_{\mu'\nu'\mu\nu}^* = \sum_j \frac{\partial \lambda_j}{\partial q} (Q_j^{20})_{\mu\nu}^*, \quad (9)$$

$$\sum_{\mu' < \nu'} Z_{\mu'\nu'}^* B_{\mu'\nu'\mu\nu} + Z_{\mu'\nu'} A_{\mu'\nu'\mu\nu}^* = \sum_j \frac{\partial \lambda_j}{\partial q} (Q_j^{20})_{\mu\nu}.$$

To simplify the notation it is convenient to introduce indexes ρ and σ corresponding to the pair of indexes μ and ν with the restriction $\mu < \nu$. The ordering of the correspondence is irrelevant in what follows. With the new indexes, $Z_{\mu\nu}$ becomes the vector Z_{ρ} and the four index quantities $A_{\mu'\nu'\mu\nu}$ become the matrix elements of a hermitian matrix $A_{\rho'\rho}$. The same applies to the $B_{\mu'\nu'\mu\nu}$ that become the matrix elements of a symmetric matrix $B_{\rho'\rho}$. In terms of the new indexes the previous equation becomes

$$\sum_{\rho'} Z_{\rho'}^* A_{\rho'\rho} + Z_{\rho'} B_{\rho'\rho}^* = \sum_j \frac{\partial \lambda_j}{\partial q} (Q_j^{20})_{\rho}^*, \quad (10a)$$

$$\sum_{\rho'} Z_{\rho'}^* B_{\rho'\rho} + Z_{\rho'} A_{\rho'\rho}^* = \sum_j \frac{\partial \lambda_j}{\partial q} (Q_j^{20})_{\rho}. \quad (10b)$$

Introducing the linear response matrix (LRM) \mathbb{L}

$$\mathbb{L} = \begin{pmatrix} A & B \\ B^* & A^* \end{pmatrix}, \quad (11)$$

which is closely related to the matrix appearing in the Random Phase Approximation (RPA), it is easy to express Z in terms of the partial derivatives of the chemical potentials

$$\begin{pmatrix} Z \\ Z^* \end{pmatrix} = \mathbb{L}^{-1} \sum_j \frac{\partial \lambda_j}{\partial q} \begin{pmatrix} Q_j^{20} \\ Q_j^{20*} \end{pmatrix}. \quad (12)$$

The partial derivatives of the chemical potentials are determined by plugging the above result in the definition of the constraints

$$\langle \Phi(q_j + \delta q) | \hat{Q}_i | \Phi(q_j + \delta q) \rangle = q_i + \delta_{ij} \delta q. \quad (13)$$

As a consequence of this requirement we get

$$\frac{\partial \lambda_i}{\partial q_j} = \left(M_{(-1)}^{-1} \right)_{ij}, \quad (14)$$

where the quantity $(M_{(-1)})_{ij}$ is given by

$$(M_{(-1)})_{ij} = (Q_i^{20*} Q_j^{20}) \mathbb{L}^{-1} \left(\begin{matrix} Q_j^{20} \\ Q_j^{20*} \end{matrix} \right). \quad (15)$$

Collecting together all the partial results we finally obtain

$$\left(\begin{matrix} p_{q_j}^{20} \\ -p_{q_j}^{20*} \end{matrix} \right) = -i \sum_k \left(M_{(-1)}^{-1} \right)_{kj} \mathbb{L}^{-1} \left(\begin{matrix} Q_k^{20} \\ Q_k^{20*} \end{matrix} \right). \quad (16)$$

The evaluation of the momentum matrix elements requires the inversion of \mathbb{L} which is in general a tremendous task, given the typical number of two quasiparticle excitations involved in a realistic calculation. An alternative (and useful) expression for the momentum operator (or Z) can be obtained by evaluating the derivatives of the densities (both normal and abnormal) with respect to the constraints (see Appendix).

2.2. The Generator Coordinate Method inertia

The GCM does not directly provide an expression of the collective inertia. It is only after introducing some local approximation that the Hill–Wheeler equation can be reduced to a collective Schrödinger equation and yield the associated inertia [10]. Traditionally, the GOA is the approximation of choice to make this connection.

Assuming that the width of the Gaussian does not depend on q the GCM–GOA mass is given by [1,6,10]

$$\frac{1}{M_{\text{GOA}}} = -\frac{1}{4\gamma^2} (h_{qq} + h_{q'q'} - 2h_{qq'}), \quad (17)$$

where $h_{qq} = \frac{\partial^2}{\partial q^2} h(q, q')|_{q=q'}$, $h_{q'q'} = \frac{\partial^2}{\partial q'^2} h(q, q')|_{q=q'}$ and $h_{qq'} = \frac{\partial^2}{\partial q \partial q'} h(q, q')|_{q=q'}$ with

$$h(q, q') = \frac{\langle \phi(q) | \hat{H}_{\text{eff}} | \phi(q') \rangle}{\langle \phi(q) | \phi(q') \rangle}. \quad (18)$$

Here $\hat{H}_{\text{eff}} = \hat{H} - \lambda_N(\hat{N} - N) - \lambda_Z(\hat{Z} - Z)$ as required to preserve particle number on the average also for the GCM wave functions [11,12]. If the constant width is not assumed [13,11,12] the above expression remains valid, but one has to replace the partial derivatives by covariant ones that include in their definition the affine connection or Christoffel symbols of differential geometry. We will use in the following the constant width formula to preserve the traditional connection with the momentum operator defined above. Assuming time reversal invariant states $|\phi(q)\rangle$ such that $\langle \phi(q) | \frac{\partial}{\partial q'} | \phi(q') \rangle|_{q=q} = 0$ and computing second derivatives of the HFB states as

$$\frac{\partial^2}{\partial q^2} |\phi(q)\rangle = \lim_{\delta q \rightarrow 0} \frac{1}{\delta q^2} (|\phi(q + \delta q)\rangle + |\phi(q - \delta q)\rangle - 2|\phi(q)\rangle),$$

with $|\phi(q + \delta q)\rangle = \mathcal{N}(q)(1 + \delta q \hat{Z} + \frac{1}{2} \delta q^2 \hat{Z}^2 + \dots)|\phi(q)\rangle$ (curvature terms $\frac{\partial^2 Z}{\partial q^2}$ [14] are omitted) we finally obtain

$$h_{qq} = \langle \phi(q) | \left(\hat{Z}^\dagger \right)^2 \Delta \hat{H}_{\text{eff}} | \phi(q) \rangle = \sum_{\rho\rho'} Z_\rho^* Z_{\rho'}^* B_{\rho\rho'},$$

$$h_{q'q'} = \langle \phi(q) | \Delta \hat{H}_{\text{eff}} \hat{Z}^2 | \phi(q) \rangle = \sum_{\rho\rho'} Z_\rho Z_{\rho'} B_{\rho\rho'}^*,$$

$$h_{qq'} = \langle \phi(q) | \hat{Z}^\dagger \Delta \hat{H}_{\text{eff}} \hat{Z} | \phi(q) \rangle = \sum_{\rho\rho'} Z_\rho^* Z_{\rho'} A_{\rho\rho'},$$

that leads to the compact expression

$$\frac{1}{M_{\text{GOA}}} = \frac{1}{4\gamma^2} \begin{pmatrix} Z^* & Z \end{pmatrix} \begin{pmatrix} A & -B \\ -B^* & A^* \end{pmatrix} \begin{pmatrix} Z \\ Z^* \end{pmatrix}. \quad (19)$$

Please note that the A and B matrices above are not exactly the same as those of Eqs. (8) which are defined in terms of \hat{H}' instead of \hat{H}_{eff} . The differences, associated with the collective constraints, are zero for the ground state and very small elsewhere as we have checked in our example below. In the following we will assume them to be the same. Using the definition of Z , \mathbb{L} and introducing the matrix $\eta = \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}$ we finally obtain

$$\frac{1}{M_{\text{GOA}}} = \frac{1}{4} \gamma^{-1} M_{(-1)}^{-1} \bar{M}_{(-1)} M_{(-1)}^{-1} \gamma^{-1},$$

that is written in a way that can be easily generalized to the multidimensional case. The $\bar{M}_{(-1)}$ is given by

$$\bar{M}_{(-1)lm} = \begin{pmatrix} Q_l^{20*} & Q_l^{20} \end{pmatrix} \mathbb{L}^{-1} \eta \mathbb{L} \eta \mathbb{L}^{-1} \begin{pmatrix} Q_m^{20} \\ Q_m^{20*} \end{pmatrix}. \quad (20)$$

The width γ can be obtained in a similar manner:

$$\begin{aligned} \gamma &= \frac{\partial^2}{\partial q \partial q'} \langle \phi(q) | \phi(q') \rangle|_{q=q'} = \langle \phi(q) | \hat{Z}^\dagger \hat{Z} | \phi(q) \rangle \\ &= \sum_\rho |Z_\rho|^2 = \frac{1}{2} M_{(-1)}^{-1} M_{(-2)} M_{(-1)}^{-1}, \end{aligned} \quad (21)$$

where $M_{(-2)}$ is defined in analogy with Eq. (15) but replacing \mathbb{L}^{-1} by \mathbb{L}^{-2} . In the non-perturbative cranking approach we use in Eq. (19) the Z obtained from the partial derivatives of the density matrix and pairing tensor (see Eq. (A.8)). Additionally, we use the cranking approximation for \mathbb{L} where $B = 0$ and A is replaced by its diagonal approximation $A_{\rho\rho'} = E_\rho^{2qp} \delta_{\rho\rho'}$ with $E_\rho^{2qp} = E_\mu + E_\nu$. Inserting this approximation into the general equation we arrive to

$$\frac{1}{M_{\text{GOA}}^{\text{NP}}} = \frac{\sum_{\mu < \nu} (E_\mu + E_\nu) |Z_{\mu\nu}|^2}{2 \left(\sum_{\mu < \nu} |Z_{\mu\nu}|^2 \right)^2}, \quad (22)$$

that is the expression used in this paper. We do not use BCS like approximations like the one discussed in Ref. [7].

2.3. Density dependent forces

For density dependent forces like Gogny or Skyrme the above formulation has to be slightly modified. In Eq. (4) the Hamiltonian $\hat{H}(q + \delta q)$ has to be replaced by $\hat{H}(q + \delta q) + \partial \hat{H}(q + \delta q)$ where the one body rearrangement term is given by $\partial \hat{H}(q + \delta q) = \sum_{ij} \partial \Gamma(q + \delta q)_{ij} c_i^\dagger c_j$ with matrix elements

$$\partial \Gamma(q + \delta q)_{ij} = \langle \Phi(q + \delta q) | \frac{\delta \hat{H}}{\delta \rho} \varphi_i^*(\vec{r}) \varphi_j(\vec{r}) | \Phi(q + \delta q) \rangle. \quad (23)$$

When expressing those quantities in terms of the corresponding ones at deformation q , derivatives with respect to q of both $\hat{H}(q)$

and $\partial\hat{\Gamma}(q)$ have to be considered. The expressions obtained are rather involved but straightforward to derive and they will not be given here. In addition, those derivatives only enter the LRM and therefore they are not required in the non-perturbative case except for the definition of the one-quasiparticle energies that must be computed with the Hamiltonian including the rearrangement term $\hat{H}(q) + \partial\hat{\Gamma}(q)$.

2.4. The GCM-GOA inertia

To compute the GCM-GOA inertia without using the cranking approximation we use Eq. (17) evaluating the derivatives numerically. The required Hamiltonian overlap in Eq. (18) is evaluated using the expressions of the generalized Wick theorem [15]. For the phenomenological density dependent part of the Gogny force we use the mixed density prescription as discussed in Refs. [16,17]. First order finite difference formulas are used for the second derivatives ($f''(x) = (f(x+h) + f(x-h) - 2f(x))/h^2$) with a value of h conveniently chosen according to the collective variable used (see below). The width γ is computed numerically in the same way from the norm overlap.

2.5. The Adiabatic Time Dependent HFB inertia

The ATDHFB inertia [18] can be evaluated using the same framework as above, but imposing additional constraints on the momentum operators [19]. We are not going to provide the details here, but following the same steps as above in the quasiparticle picture one gets

$$M_{lm}^{\text{ATDHFB}} = (P_l^{20*} \ P_l^{20}) \mathbb{L}^{-1} \begin{pmatrix} P_m^{20} \\ P_m^{20*} \end{pmatrix}. \quad (24)$$

Introducing the matrix

$$\bar{M}_{(-3)lm} = (Q_l^{20*} \ Q_l^{20}) \mathbb{L}^{-1} \eta \mathbb{L}^{-1} \begin{pmatrix} Q_m^{20} \\ Q_m^{20*} \end{pmatrix}, \quad (25)$$

which is very similar in structure to $\bar{M}_{(-1)lm}$ of Eq. (20), we obtain

$$M_{(-1)lm}^{\text{ATDHFB}} = M_{(-1)}^{-1} \bar{M}_{(-3)} M_{(-1)}^{-1}. \quad (26)$$

A method for the exact evaluation of the ATDHFB inertia has been formulated in [20] and applied to very simple cases. A more recent attempt based on a direct evaluation of the LRM and its numerical inversion seems to be rather impractical due to the enormous computational cost [21]. Recently, it has been suggested [22] that the finite amplitude method [23] could be useful for this task, but so far, it has only been applied to the evaluation of the Thouless–Valatin moment of inertia.

2.6. The perturbative approximation

In the perturbative cranking approximation the \mathbb{L} matrix is approximated by its diagonal also in the definition of the momentum operator Eq. (16). The approximate \mathbb{L} commutes with η and the quantity defined in Eq. (20) becomes the $M_{(-1)}$ defined in Eq. (15) which in turn becomes $M_{(-1)}^{\text{PE}}$ with the momenta or order n defined as

$$(M_{(-n)}^{\text{PE}})_{ij} = \sum_{\mu < \nu} \frac{(Q_i^{20*})_{\mu\nu} (Q_j^{20})_{\mu\nu} + h.c.}{(E_\mu + E_\nu)^n}. \quad (27)$$

In the perturbative approximation the $\bar{M}_{(-3)}$ of Eq. (25) becomes $M_{(-3)}^{\text{PE}}$ and the $M_{(-2)}$ in the definition of the width Eq. (21) becomes $M_{(-2)}^{\text{PE}}$.

2.7. Connection with rotational band moments of inertia and inequalities

We would like to mention the similarity between the non-perturbative inertias and the Inglis–Belyaev and approximate Yoccoz moments of inertia [10]. In this case, the “momentum operator” is dictated by symmetry considerations (it is the J_x operator) and therefore the approximate expressions used in the literature to compute moments of inertia fall into the non-perturbative cranking category discussed here [10]. Concerning the exact moments of inertia, the Thouless–Valatin moment of inertia is obtained in a similar framework to the ATDHFB case, whereas the Yoccoz moment of inertia corresponds to the GCM-GOA inertia. A comparison of the two moments of inertia [14,24] reveals that the Thouless–Valatin is typically a factor 1.4 larger than the Yoccoz one both when computed exactly and when computed in the non-perturbative cranking spirit.

In [25] it was shown, using the Schwarz inequality, that at the minima of the potential energy surface the exact inertias satisfy $M_{\text{ATDHFB}}^{\text{ATDHFB}} \geq M_{\text{GCM}}^{\text{GCM}}$. The same inequality was proved true for the whole fission path in the case of the perturbative inertias. In the case of the non-perturbative inertias and following the same arguments as in [25] it is straightforward to show that the same inequality also applies.

3. Results

In this section we compare the numerical results obtained for the quadrupole collective inertia in the typical case of the fission of the actinide ^{234}U .

In Fig. 1 the results for ^{234}U are shown as a function of the mass quadrupole moment Q_{20} expressed in barns. In panel a) the potential energy surface, given by the HFB energy, is depicted: the characteristic normal deformed minimum at $Q_{20} = 12\text{ b}$ ($\beta_2 = 0.25$) is obtained, followed by a fission isomer (or superdeformed state) at $Q_{20} = 40\text{ b}$ ($\beta_2 = 0.71$) with an excitation energy of 4.2 MeV. A very broad and high (9.5 MeV) second fission barrier is found next. In panel b) the particle–particle energy E_{pp} defined as $\frac{1}{2}\text{tr}(\Delta^*\kappa)$ is given separately for protons (full) and neutrons (dashed). A rather intricate behavior is observed with the quadrupole moment, due to different level crossings that increase or decrease the level density around the Fermi level. The collective inertias [ATDHFB, panel c)] and [GCM-GOA, panel d)] are also given in the figure. The full and dashed lines represent the non-perturbative (NP) and perturbative (PE) cranking results, respectively. Full lines labeled with the values 0.05 b, 0.1 b and 1 b represent calculations with different values of the step size δQ_{20} used to evaluate the derivatives numerically. The different curves sit one on top of each other indicating a satisfactory convergence of the method.

Two main conclusions regarding the collective inertias can be extracted from panels c) and d). The first one is that the $\text{ATDHFB}_{\text{np}}$ and $\text{GCM-GOA}_{\text{np}}$ cranking inertias have exactly the same peak structure. As expected (see the discussion in Sec. 2.7), and in both the NP and PE cases, the ATDHFB mass is larger than the GCM-GOA one, as shown in panel e). What is remarkable is that in the two numerical schemes (NP and PE) the ATDHFB and GCM-GOA inertias differ by a factor around 1.5 and rather constant over the whole deformation range up to the region corresponding to two separate fragments ($Q_{20} > 126\text{ b}$). After this point on the quadrupole moment has a geometric origin (being proportional to the square of the distance between the two fragments) and the $\text{ATDHFB}_{\text{np}}/\text{GCM-GOA}_{\text{np}}$ ratio remains very close to one. We also point out that the 1.5 value of the ratio is consistent with other

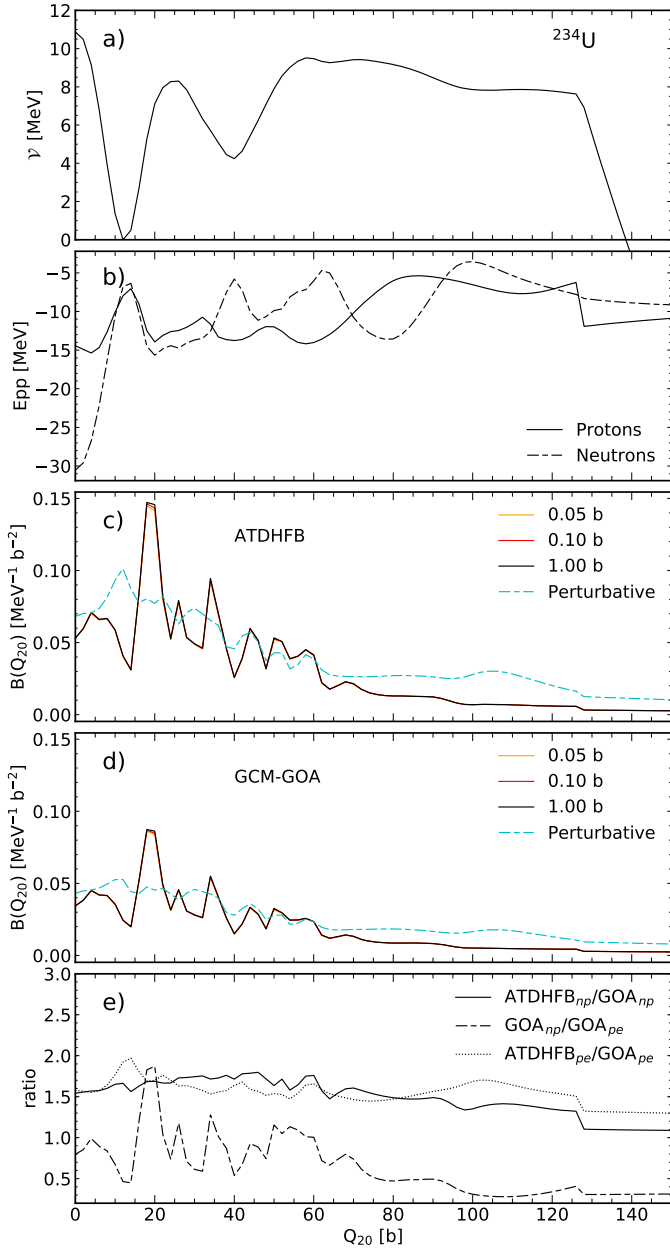


Fig. 1. Fission results for the nucleus ^{234}U shown as a function of Q_{20} (b). In panel a) the HFB energy is given. The particle–particle proton (full) and neutron (dashed) energies are plotted. In panels c) and d) the ATDHFB and GCM-GOA inertias, respectively, are shown in the perturbative (blue dashed) and non-perturbative (full lines) approaches. In the non-perturbative case, we observe several overlaid curves corresponding to different values of a parameter used in the numeric evaluation of the momentum operator. In panel e) the ratios ATDHFB to GCM-GOA inertias (NP, full line, PE dotted line) and GCM-GOA_{np} to GCM-GOA_{pe} are shown.

studies concerning the values of the Thouless–Valatin and Yoccoz moments of inertia (see section 2.7). The second finding is that both the ATDHFB_{np} and GCM-GOA_{np} inertias have more pronounced peaks compared to the perturbative calculations. Looking at the variations of the particle–particle energy E_{pp} it is possible to relate these peaks with a larger sensitivity of the non-perturbative inertias to the presence of level crossings. This “lack of adiabaticity” of the non-perturbative inertias is consistent with the ATDHFB results of Baran et al. [7]. Finally, the fluctuations of the GCM-GOA_{np}/GCM-GOA_{pe} ratio depicted in panel e) (dashed line) suggest that the recipe of multiplying the perturbative inertia by a

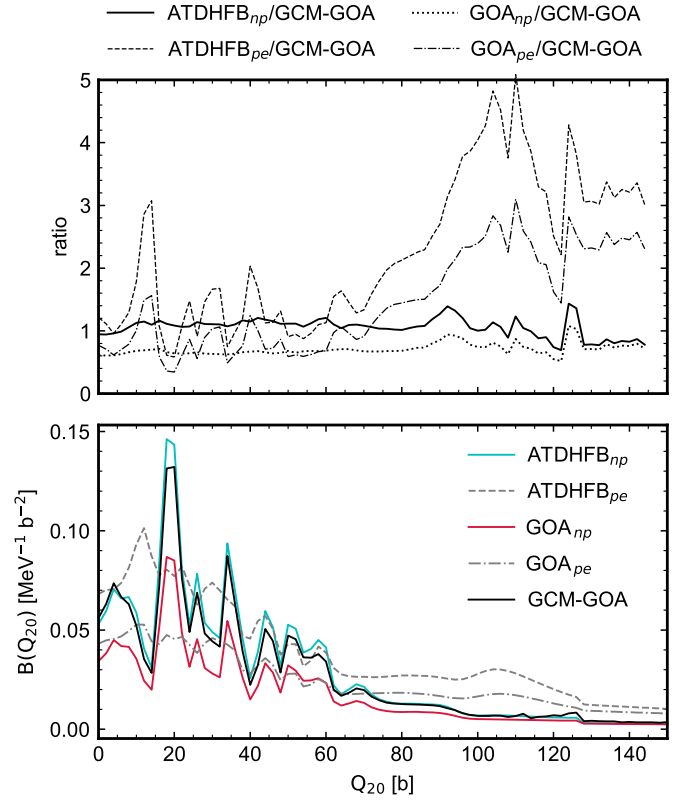


Fig. 2. Upper panel: Ratios of different computed inertias, as a function of the quadrupole moment and for the nucleus ^{234}U . Lower panel: The values of the different inertias as a function of the quadrupole moment.

constant factor in order to simulate the non-perturbative masses is not a reasonable assumption [26].

The agreement between the non-perturbative inertias diminishes the uncertainties arising from the ambiguity in the choice of the theoretical scheme (ATDHFB vs GCM-GOA), but still the suitability of this numerical approximation has to be proved. In order to address this point we computed the exact GCM-GOA collective inertias (GCM-GOA) and compared the results with the perturbative and non-perturbative calculations. The lower panel of Fig. 2 shows the different inertias computed in this work and the upper panel represents the ratio of the perturbative and non-perturbative calculations to the exact GCM-GOA collective inertias. Surprisingly the GCM-GOA inertias have the same peak structure and evolution with quadrupole deformation of the non-perturbative calculations, with a ATDHFB_{np}/GCM-GOA ratio very close to one (or equivalently GCM-GOA_{np}/GCM-GOA ~ 0.6) and virtually independent of Q_{20} . This result brings consistency to the nuclear fission theory, indicating that the GCM-GOA inertia can be obtained either by using the ATDHFB_{np} scheme or the GCM-GOA_{np} mass multiplied by a constant factor around 1.5. On the other hand, the upper panel of Fig. 2 shows that the ratio of perturbative cranking to GCM-GOA masses depends on the quadrupole deformation, with discrepancies in some cases as large as a factor of 5. This comparison confirms the results found in the non-perturbative study and indicating the inadequacy of multiplying the perturbative inertias by a phenomenological factor to grasp the structure of the exact GCM-GOA collective inertia [26].

4. Conclusion

In summary, this work provides a solution to the uncertainties arising from the ambiguity in the choice of both the theoretical

framework and the numerical approximations involved in the calculation of collective inertias. Taking ^{234}U as a benchmark, the non-perturbative cranking and exact collective inertias were calculated for the first time using the Generator Coordinate Method (GCM) in the Gaussian overlap approximation (GOA) and compared with the Adiabatic Time Dependent Hartree Fock Bogolyubov (ATDHFB) non-perturbative and perturbative cranking inertias.

The ATDHFB $_{np}$, GCM-GOA $_{np}$ and GCM-GOA inertias present the same peak structure along the whole fission path, being the GCM-GOA $_{np}$ calculations smaller by a roughly constant factor around 1.5. These inertias show a much richer structure compared to the perturbative calculations indicating a stronger sensitivity to level crossings. These results are not only important for fission but also for approximate models used to describe collective dynamics within the Bohr Hamiltonian or the Collective Schrödinger equation. The use of the non-perturbative inertias along with a phenomenological stretching factor can be a good substitute for the more elaborated beyond mean field calculations with the GCM-GOA. It would be highly desirable to extend this comparison to the exact ATDHFB inertia, but the complications arising from the calculation of the inverse of the linear response matrix \mathbb{L} prevent this comparison for the moment. Work aimed to compute exact ATDHFB inertias is under way and will be reported elsewhere.

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Appendix A. Derivatives of the density matrix

The relationship between the momentum operator matrix elements and the derivative of the densities with respect to the constraints is established. Let us consider the density $\rho_{ij}(q)$ and the pairing tensor $\kappa_{ij}(q)$ corresponding to a set of values of the constraints q . By shifting one of the constraints q_k by an infinitesimal δq we have to consider

$$\rho_{ij}(q_k + \delta q) = \frac{\langle \phi(q_k + \delta q) | c_j^\dagger c_i | \phi(q_k + \delta q) \rangle}{\langle \phi(q_k + \delta q) | \phi(q_k + \delta q) \rangle}. \quad (\text{A.1})$$

With Eqs. (2), (3) and the contractions $\langle \phi(q) | c_j^\dagger \beta_\mu^\dagger | \phi(q) \rangle = V_{j\mu}$ and $\langle \phi(q) | c_j \beta_\mu^\dagger | \phi(q) \rangle = U_{j\mu}$ we easily arrive to

$$\frac{\partial \rho_{ij}}{\partial q_k} = \left(U Z_k V^T - V^* Z_k^* U^\dagger \right)_{ij} \quad (\text{A.2})$$

and

$$\frac{\partial \kappa_{ij}}{\partial q_k} = \left(U Z_k U^T - V^* Z_k^* V^\dagger \right)_{ij}. \quad (\text{A.3})$$

In order to solve for Z_k in the above expressions it is far more convenient to work with the unitary block matrix W of Bogoliubov amplitudes

$$W = \begin{pmatrix} U & V^* \\ V & U^* \end{pmatrix} \quad (\text{A.4})$$

and the associated generalized density matrix

$$\mathcal{R} = \begin{pmatrix} \rho & \kappa \\ -\kappa^* & 1 - \rho^* \end{pmatrix}. \quad (\text{A.5})$$

Using them we can write the expressions for the derivatives in a compact way as

$$\frac{\partial \mathcal{R}}{\partial q_k} = W \begin{pmatrix} 0 & Z_k \\ -Z_k^* & 0 \end{pmatrix} W^\dagger, \quad (\text{A.6})$$

that can straightforwardly be solved for Z

$$\begin{pmatrix} 0 & Z_k \\ -Z_k^* & 0 \end{pmatrix} = W^\dagger \frac{\partial \mathcal{R}}{\partial q_k} W, \quad (\text{A.7})$$

leading to

$$Z_k = U^\dagger \frac{\partial \rho}{\partial q_k} V^* + U^\dagger \frac{\partial \kappa}{\partial q_k} U^* - V^\dagger \frac{\partial \kappa^*}{\partial q_k} V^* - V^\dagger \frac{\partial \rho^*}{\partial q_k} U^*. \quad (\text{A.8})$$

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